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METHOD FOR PRODUCING A MAGNETIC DEVICE

5 Cross Reference to Related Applications:

This is a divisional of U.S. application No. 09/756,530, filed January 10, 2002, which was a continuation of International application number PCT/DE99/01950, filed July 1, 1999, which designated the United States, and which was not published in English.

Background of the Invention:

Field of the Invention:

The present invention relates to a method for producing a magnetic device in environments where, for example it is 15 desired to provide for or against the passage of electromagnetic radiation. Such applications may range from a shielding for a cable to a plastering for a wall of a room or rooms. While the present invention will be described with respect to the latter example, applications of the present 20 invention is limited only by the imagination of one skilled in the art. The present invention relates particularly to magnetic material grain size. The related art sets out two examples of consideration of grain size in production and 25 applications.

Reference WO 92/08678 A1 concerns a magnetized product formed by the hardening of cement and water into a malleable mass. Such mass contains granular magnetic materials, including soft iron, thereby displaying certain magnetic properties. The material may be applied in electrical dynamos.

Reference EP 0393599 B1 sets out a surface mounted electrical coil which may be surrounded by a product of synthetic material wherein a powdery magnetic material such as carbonyl iron or ferrite is deposited.

Summary of the Invention:

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Ferromagnetism refers to the physical phenomenon wherein certain electrically uncharged materials strongly attract others. Ferromagnetic materials, when exposed to magnetic fields, become easily magnetized and otherwise display strong magnetic properties. The magnetism in ferromagnetic materials is caused by the alignment patterns of the materials constituent atoms, which act as elementary electromagnets. Ferromagnetic material may be considered as comprising a large number of smaller regions, or domains, wherein the atomic or ionic magnetic moments are aligned. Where the combined

ferromagnetic material will not display any significant

magnetic properties. However, when an external magnetic field is applied, the moments will rotate into alignment with the

moments of the domains are randomly oriented, the

field, thereby reinforcing one another and causing magnetic properties of the material as a whole to be displayed. Such alignment continues until a point of saturation, particular to individual ferromagnetic materials. Examples of such materials includes, iron, cobalt, nickel, alloys or compounds containing each, along with some rare earth metals, as known to one skilled in the art.

Ferrite is a ceramic-like ferromagnetic material having a variety of applications. A determining factor of ferrite grain size, in a given material, is its initial permeability which refers to the initial slope of the magnetic flux density (8), established within the material by a magnetizing field, versus the magnetic field strength (H) of the magnetizing field. The slope is typically characteristic of an unmagnetized ferromagnetic material and otherwise represents the magnetic permeability under very small-applied magnetic fields. Magnetic permeability refers to the relative increase or decrease in the resultant magnetic field inside a particular material as compared with the magnetizing field wherein the material may be located. Magnetic permeability is typically assigned the Greek character mu and defined as B/H.

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Returning to ferrite, a determination of essential grain size is the initial permeability. The initial permeability of a solid including ferrite therein depends on the ferrite grain

size diameter and its relative size with respect to domains of the solid material. A typical domain has a diameter of about 0.5 microns. Where the average grain diameter size of ferrite approaches the size of the domain, initial permeability is reduced. The reduction occurs because the number of domains per grain dramatically drops, such that the alignment of the domains in response to an applied magnetic field discontinues.

It is therefore an object of the invention to set out a method for making it of ferromagnetic material having an elevated or maximized initial permeability. In particular, the material is applicable to shielding for frequencies of above 100 kHz, and in particular 1 MHz to 2 GHz. It is another object of the invention to provide a method which can be implemented so as to enable mass production at reasonable engineering effort and expense and with maximally replicable component characteristics.

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The present invention comprises a magnetic device comprising a plurality of ferromagnetic material grains, said grains having a minimum diameter larger than an average domain diameter of said grains, and said grains further embedded in a matrix.

The present invention further comprises a method for producing a magnetic device, comprising the steps of: forming ferromagnetic grains, said grains having an average diameter greater than domains of said grains; and embedding said grains

in a matrix, said matrix comprising a hardening material.

Other features which are considered as characteristic for the invention are set forth in the appended claims.

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Although the invention is illustrated and described herein as embodied in a method for producing a magnetic device, it is nevertheless not intended to be limited to the details shown, since various modifications and structural changes may be made therein without departing from the spirit of the invention and within the scope and range of equivalents of the claims.

The construction and method of operation of the invention, however, together with additional objects and advantages thereof will be best understood from the following description of specific embodiments when read in connection with the accompanying drawings.

Brief Description of the Drawings:

- Fig. 1 is a sectional view of the present invention as applied to plaster for a wall;
 - Fig. 2 is an enlarged view of a portion of Figure 1;
- Fig. 3 is a sectional view of the present invention as applied to shielding for a magnetic disk

Fig. 4 is a cross section of the magnetic disk depicted in Fig. 3

Fig. 5 is a diagram depicting permeability of materials applied in accordance with the present invention; and

Fig. 6 is a second diagram depicting permeability materials applied in accordance with the present invention.

10 Description of the Preferred Embodiments:

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The following sets out an embodiment of the present invention, wherein like reference numerals refer to equivalent functioning elements. Figs. 1 and 2 depict a similar embodiment of the present invention, namely, application of the invention in a plaster for covering a wall. As shown in 15 Fig. 1, a wall 1 is covered with a plaster 2. The plaster, as will be detailed below, is a shielding against particular electromagnetic frequencies common to modern telecommunications, namely 100kHz and above. The wall itself may be of any suitable construction envisioned by the skilled 20 artisan, including layers of bricks, cement, and the like. The plaster 2 comprises a shielding and contains grains of ferrite embedded in a matrix. The ferrite may be sintered, iron and the like. Fig. 2 sets out a portion of the shielding, II, in more detail. As shown therein, the shield 25 2, comprises a plurality of ferrite grains 3, 4 arranged in a

matrix 5 of hardened cement. The matrix may comprise equivalent materials envisioned by the skilled artisan to effectively accommodate a ferromagnetic material, such as ferrite, in a shielding matrix formation. The depicted grains 3, 4 have essentially larger diameters than a typical domain diameter of ferrite, namely 0.5 microns. As such, a relatively high initial permeability for the shielding 2 is effected. The size of the grains 3, 4 may range up to 10 millimeters thereby effecting the depicted non-homogeneous shield 2. The grains may have a minimum diameter of about 10 microns and an overall total average diameter of about 100 microns. The shield may comprise 5 parts cement, 5 parts water, and 100 parts grains. Hence the shield may have at least 80% grain density, and preferably about 90-95% grain density.

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In the depicted embodiment, the shielding 2 includes a first number of grains 3 and a second number of grains 4. The first number of grains has an average diameter of about 8 mm and the second number of grains includes an average diameter of about 2 mm. Taken as a group, the discrepancy among the diameters can be relatively high, as for example, for grains 3, the range may be between about 1 mm and 12 mm and for grains 4, the range may be between about 0.1 mm and 6 mm. The depicted matrix may be constructed of cement, as may be manufactured by AALBOG PORTLAND A/S of Aalborg, Denmark and may include fine-

granular component material such as silizimudioxide, aluminum oxide, calcium and other related materials as well as a surface active medium to elevate the flow ability of the cement ferrite matrix mass. An advantageous arrangement includes using cement, which requires relatively little water, as compared with other available cements, so as to avoid pores within the matrix 5.

Figs. 3 and 4 depict a magnetic disk manufactured according to

the present invention. Herein the disk, preferably a magnetic

disk, includes an electromagnetic field with the above

frequencies (above 100 kHz) and manufactured with the

equivalent materials discussed above with respect to Figures 1

and 2. Other applications may include a coil, circuit and the

like.

Fig. 5 depicts the initial permeability of a product built according to the above specifications versus the percentage or density of ferrite. The abscissa refers to permeability while the ordinate refers to the ferrite percentage. Fig. 6 depicts the interdependence of permeability with frequency of a magnetic field impinging upon a solid. The permeability is in essence a complex valence of the influence of the magnetic field upon the solid. The real component of the graphed permeability, as depicted in Fig. 5, is in effect a proportion of magnetic flux density B and magnetic field strength H as

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impinging upon the solid. The imaginary component of the graphed permeability sets out dampening or absorption of the magnetic field as applied to the product. Where such loss becomes substantial, a dispersion effect is made upon the magnetic field.

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Continuing with Fig. 6, here the effects on a magnetic field of two products of slight composition variation, is depicted. In particular, the imaginary and real components of the permeability measurements discussed above. Like letters refer to like products. The abscissa represents the real and imaginary components of permeability and the ordinate represents a logarithmic scale of frequency. The curves not beginning at the origin refer to the real component of permeability, while the curves beginning at the original refer to the imaginary component. As depicted, at lower frequencies, the real components are practically constant, while the imaginary components are relatively non-existent. At frequencies about 10MHz, the real components begin to ascend while the imaginary components climb. As such, about 100 MHz, the impinging magnetic field essentially becomes dispersed. Hence, products constructed with the above ferrite density and size effectively shield at about 100 MHz. shielding is particularly useful in the telecommunication arts as the frequencies lie in the pulse range of conventional microprocessors as well as conventional mobile radio units.

The invention being thus described, it will be obvious that
the same may be varied in many ways. Such variations are not
to be regarded as a departure from the spirit and scope of the
invention, and all such modifications would be obvious to one
skilled in the art are intended to be included within the
scope of the following claims.